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| Vol. 11, No. 9, 2021, Pg. 162 - 172              |                  |
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# Design and Optimization of Piezoelectric Cantilever for Energy Harvesting Application by Using Taguchi Method

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### Abstract

Piezoelectric element is one of the best innovation and technologies to be utilized in energy harvesting to produce electrical energy from vibrations. It can give a perfect and independent arrangement solution that can be stored and used to power some wireless sensors, electronic device, and other low-power applications. With this goal in mind, a design and optimization of piezoelectric cantilever beam for energy harvesting has been developed. The focus of this paper is to discuss the design and optimization of piezoelectric cantilever beam by using Taguchi method for determine the optimal design parameters. For this study, the design of the bimorph piezoelectric harvester was performed by COMSOL software. Three parameters which are load resistance, width and length of piezoelectric cantilever has been considered. The parameters were optimized by using L16 orthogonal array Taguchi method. Optimization results showed that load resistance, width and length were found to be  $10k\Omega$ , 17mm, and 23mm respectively. The optimized outputs are 1.78mW electrical power at 5.97V for resonant frequency of 65Hz.

Keywords: Piezoelectric, Energy Harvester, Cantilever, Taguchi Method, COMSOL

### Introduction

Energy harvesting (EH) or energy scavenging is a process of capturing small amount of energy from ambient environment through various sources of energy. Engineers are challenged to design state-of-the-art systems which beneficial to humankind and power themselves from available ambient energy. Harvesters can be used as battery rechargers in various places, such as industries, houses and wearable devices (Torah et al., 2008). To date, energy harvesting have drawn great attention for wireless sensor networks power to solve a series of problems such as short life span, size and pollution. Piezoelectric devices have proven to be a potential source of power generation (Marusiak, 2012).

There are three main components in piezoelectric ambient vibration energy harvesting system as shown in Figure 1. The three main components are rectifier, voltage regulator, and energy storage device. Rectifier is used to convert alternating current (AC) to direct current (DC). Full wave bridge rectifiers is the most frequently used AC-DC rectifier for the energy

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harvesting systems (Al-Ashtari, 2013; Kalyanaraman & Babu, 2010; Sodano et al., 2005a). Next, the voltage regulator is used to regulate voltage levels that produced from the piezoelectric element. Since piezoelectric energy harvester yield low power output, it is not sufficient to power up the electronic devices. Hence, in the piezoelectric energy harvesting system, the harvested energy is usually first collected in a storage medium before being used by the load. The energy storage that commanly used are rechargeable batteries and capacitor (Shad Roundy et al., 2003; Sodano et al., 2005b; Zhang et al., 2016).

In energy harvesting, Han et al. investigated on synchronous rectifier and compared the performance with other existing rectifiers (Han et al., 2004). From their study, the circuit operated through two stages which are AC-DC rectifier and DC-DC converter. From their analysis, the most efficient method was synchronous rectification based on the three different rectifier circuits using simulation.

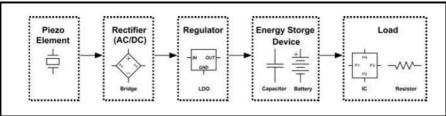


Figure 1 Block diagram of piezoelectric ambient vibration energy harvesting system

The performance of the energy harvester can be affected by different piezoelectric materials due to different piezoelectric constants. Some examples of piezoelectric materials are zinc oxide (ZnO), aluminum nitrate (AIN), lead zirconate titanate (PZT) and polyvinylidene fluoride (PVDF). Among the piezoelectric materials, PZT is the most commonly used piezoelectric material because has higher piezoelectric coefficient and high dielectric constant (Kuoni et al., 2003). According to Roundy's paper, the study focuses on modeling, design, and optimization of a piezoelectric energy harvester based on the bimorph cantilever. The cantilever was made using PZT material. Roundy observed that the design of the energy harvester must target low frequency fundamental mode compared to the higher frequency mode. This is because the potential output power is proportional to  $1/\omega$  where  $\omega$  is the frequency of the fundamental vibration mode (S. Roundy & Wright, 2004). The purpose of this paper is to research and design piezoelectric for low power device application, to run modeling and simulation of MEMS piezoelectric energy harvester using COMSOL tool and to optimize the design of piezoelectric circuit by Taguchi Method Orthogonal Array. *A. The piezoelectric cantilever configuration* 

When pressure is applied to piezoelectric materials, an electric voltage develops across the material. The two constitutive equations can model mechanical and electrical behavior (S. Roundy & Wright, 2004):

$$S = s^E T + d_t E \qquad (1)$$

 $D = d_t T + \varepsilon^T E \qquad (2)$ 

where S - mechanical strain, T - applied mechanical stress, E - Electric field, D - electric displacement,  $s^E$  - matrix of elasticity under conditions of constant electric field, d - piezoelectric coefficient matrix, and  $\varepsilon^T$ - permittivity matrix at constant mechanical strain. Large deformation can be produced by the simple structure of cantilever type energy harvesting. There are two different mode that can be used in this model of cantilever. Firstly, the 33 mode called compressive mode in which the voltage is recoverd in the three direction parallel to the direction of applied force. The other is 31 mode called transverse mode where

the voltage is recovered in one direction perpendicular to the direction of applied force. The most useful mode in harvesting applications is 31 mode because an immense proof mass would be needed for the 33 mode configuration (Lefeuvre et al., 2007).

B. Taguchi Method Orthogonal Array

One of the most comprehensive approach in product or process developments is consider design of experiments (DOE). It is a statistical approach that attempts to provide a predictive knowledge of a complex, multi-variable process with few trials (Rafidah et al., 2014). One of statistical approach is Taguchi method that can optimize the process parameters and improve the quality of components that are manufactured. Taguchi method was used to construct set of arrays called orthogonal arrays, which advocate minimum number of experiments with maximum information about all the factors that affect the outcome (Athreya & Venkatesh, 2012).

#### Methodology

#### A. Design of piezoelectric harvester

The model is designed in COMSOL software. A two dimension bimorph cantilever was consisted of two material. Lead zirconate titanate (PZT-5A) material is used as piezoelectric layer (top and bottom) and structural steel is used as substrate (middle). The energy harvester considered for the study is in the form of the cantilever shown in Figure 2. It consists of a piezoelectric bimorph with a proof mass mounted on the other end. The bimorph is grounded by embedded within it and two electrode on the exterior surface of the cantilever beam. The cantilever's dimension is 21mm length, 14mm width and 4mm x 1.7mm proof mass as shown in Table 1 (Desai et al., 2016).

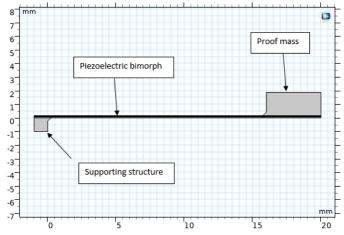


Figure 2 Configuration of bimorph piezoelectric cantilever in COMSOL

| o of the input parameters |               |
|---------------------------|---------------|
| Load resistance           | 12 kΩ         |
| Width of piezo plate      | 14 mm         |
| Length of piezo plate     | 21 mm         |
| Proof mass dimensions     | 4 mm x 1.7 mm |

#### B. Experimental design using the Taguchi method

In this study, it is considering three parameters which are load resistance, width, and length of piezo plate, with four levels for each parameter. The studied factors of the three

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parameters and four levels are given in Table 2. In full factorial experiments, 64 experiments must be performed. By using an orthogonal array suggested by Taguchi, the number of experiments needed to find the optimal parameters will be significantly reduced. Concerning the proposed parameters and levels, an L16 orthogonal array experiment was considered as shown in Table 3.

| Parameters                 | Levels |    |    |    |
|----------------------------|--------|----|----|----|
|                            | 1      | 2  | 3  | 4  |
| Load resistance (kΩ)       | 10     | 12 | 14 | 16 |
| Width of piezo plate (mm)  | 11     | 13 | 15 | 17 |
| Length of piezo plate (mm) | 20     | 21 | 22 | 23 |

| Experiment No. | Load  | Width | Length |
|----------------|-------|-------|--------|
|                | Level |       |        |
| 1              | 1     | 1     | 1      |
| 2              | 1     | 2     | 2      |
| 3              | 1     | 3     | 3      |
| 4              | 1     | 4     | 4      |
| 5              | 2     | 1     | 2      |
| 6              | 2     | 2     | 1      |
| 7              | 2     | 3     | 4      |
| 8              | 2     | 4     | 3      |
| 9              | 3     | 1     | 3      |
| 10             | 3     | 2     | 4      |
| 11             | 3     | 3     | 1      |
| 12             | 3     | 4     | 2      |
| 13             | 4     | 1     | 4      |
| 14             | 4     | 2     | 3      |
| 15             | 4     | 3     | 2      |
| 16             | 4     | 4     | 1      |

#### **Results and Discussion**

Taguchi method was used to construct a systematic approach to screen for the most sensitive input parameters that will effect the piezoelectric output parameters. Table 4 shows the effect of input parameters to the output parameters, namely the resonant frequency, voltage and electrical power. The input parameters studied are load resistance, width of piezo plate, and length of piezo plate. Figure 3 shows a sample of simulated output results for experiment run number 1 in Taguchi Orthogonal Array (Table 4).

Table 4 Taguchi Orthogonal Array showing the variation of output parameters with optimum combinations of input parameters

| Exp.<br>Run | Load<br>(kΩ) | Width<br>of<br>piezo<br>plate<br>(mm) | Length<br>of<br>piezo<br>plate<br>(mm) | Resonant<br>Frequency<br>(Hz) | Voltage<br>(V) | Electrical<br>Power<br>(mW) |
|-------------|--------------|---------------------------------------|--|-------------------------------|----------------|-----------------------------|
| 1           | 10           | 11                                    | 20                                     | 82.5                          | 4.67           | 1.09                        |
| 2           | 10           | 13                                    | 21                                     | 76                            | 5.07           | 1.28                        |
| 3           | 10           | 15                                    | 22                                     | 70                            | 5.52           | 1.52                        |
| 4           | 10           | 17                                    | 23                                     | 65                            | 5.97           | 1.78                        |
| 5           | 12           | 11                                    | 21                                     | 76                            | 5.09           | 1.08                        |
| 6           | 12           | 13                                    | 20                                     | 83                            | 4.99           | 1.04                        |
| 7           | 12           | 15                                    | 23                                     | 65                            | 6.06           | 1.53                        |
| 8           | 12           | 17                                    | 22                                     | 71                            | 5.97           | 1.48                        |
| 9           | 14           | 11                                    | 22                                     | 70                            | 5.55           | 1.10                        |
| 10          | 14           | 13                                    | 23                                     | 65                            | 6.07           | 1.32                        |
| 11          | 14           | 15                                    | 20                                     | 84                            | 5.46           | 1.06                        |
| 12          | 14           | 17                                    | 21                                     | 77.5                          | 6.03           | 1.30                        |
| 13          | 16           | 11                                    | 23                                     | 65                            | 6.02           | 1.13                        |
| 14          | 16           | 13                                    | 22                                     | 71                            | 6.02           | 1.13                        |
| 15          | 16           | 15                                    | 21                                     | 77.5                          | 6.06           | 1.14                        |
| 16          | 16           | 17                                    | 20                                     | 85                            | 6.12           | 1.17                        |

| Level | Load       | Width | Length |
|-------|------------|-------|--------|
|       | Resistance | (mm)  | (mm)   |
|       | (kΩ)       |       |        |
| 1     | 73.38      | 73.38 | 83.63  |
| 2     | 73.75      | 73.75 | 76.75  |
| 3     | 74.13      | 74.13 | 70.50  |
| 4     | 74.63      | 74.63 | 65.00  |
| Delta | 1.25       | 1.25  | 18.63  |
| Rank  | 2.5        | 2.5   | 1      |

From Table 4, it has been seen that the voltage and electrical power increase when the length and width of piezo plate increase for experiment run 1 to 4. However, the shift of resonant frequency has also changed for those experiments. Next, based on the experiments run, analysis on resonant frequency, voltage and electrical power are being analyzed as in Table 5, Table 6, and Table 7 respectively. The main effect plots are the mean response of each level factors connected by the line. When the horizontal line presents, there is no main effect present. As small deflection from horizontal, it may significantly affect the response. Steeper slope in the line illustrates the greater magnitude of the main effect.

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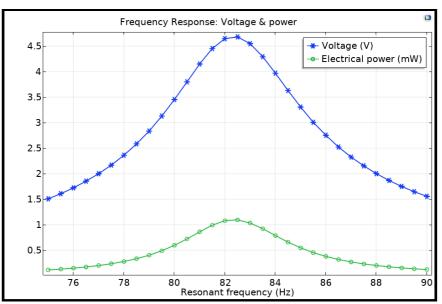


Figure 3 Simulation result for experiment run 1 using COMSOL tool.

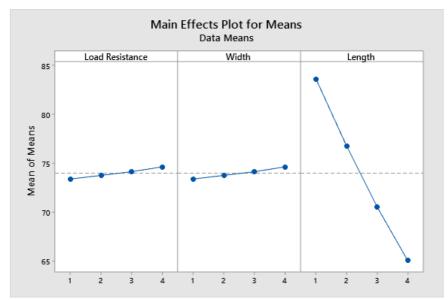


Figure 4 Graph of main effects plot for means resonant frequency versus load, width, and length

The means of resonant frequency with load, width and length of the plate are shown in Figure 4. The length of the plate has great impact on the frequency of the cantilever. The resonant frequency decreased as the length increased. The load resistance and width of the plate has least significant effect on the resonant frequency. It is concluded that the frequency is inversely proportional to the length of piezo plate.

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| Level | Load<br>Resistance | Width<br>(mm) | Length<br>(mm) |
|-------|--------------------|---------------|----------------|
|       | (kΩ)               | (11111)       | (11111)        |
| 1     | 5.308              | 5.332         | 5.310          |
| 2     | 5.527              | 5.538         | 5.563          |
| 3     | 5.778              | 5.775         | 5.765          |
| 4     | 6.055              | 6.022         | 6.030          |
| Delta | 0.747              | 0.690         | 0.720          |
| Rank  | 1                  | 3             | 2              |

Table 6 Respond table for means voltage with respect to parameters set.

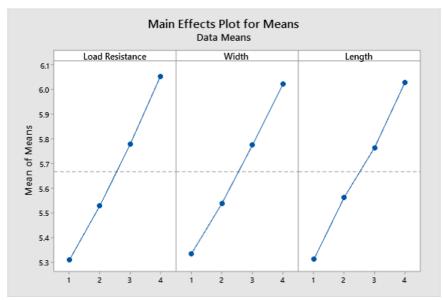


Figure 5 Graph of main effects plot for means voltage versus load, width, and length

The means of voltage with load, width and length of the plate are shown in Figure 5. The three parameters have high sensitivity on the voltage of the cantilever. Therefore, the voltage is directly proportional to the load, width, and length of piezo plate.

| Level | Load       | Width | Length |
|-------|------------|-------|--------|
|       | Resistance | (mm)  | (mm)   |
|       | (kΩ)       |       |        |
| 1     | 1.417      | 1.100 | 1.090  |
| 2     | 1.283      | 1.193 | 1.200  |
| 3     | 1.195      | 1.312 | 1.307  |
| 4     | 1.142      | 1.432 | 1.440  |
| Delta | 0.275      | 0.332 | 0.350  |
| Rank  | 3          | 2     | 1      |

Table 7 Respond table for means electrical power with respect to parameters set.

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Figure 6 Graph of main effects plot for means electrical power versus load, width, and length

The means of electrical power with load, width, and length are shown in Figure 6. The electrical power has decreased as the load resistance increased. Meanwhile, the increase of width and length have increased the electrical power. Based on the analysis, load resistance of 1.417, level 4 of width and level 4 of length were selected for the optimal design of the piezoelectric energy harvester to get high voltage and electric power at a low scale resonant frequency. The optimal value for load resistance, width and length were found to be  $10k\Omega$ , 17mm, and 23mm respectively. From Table 4, it can be observed that the electrical power is maximum value of 1.78mW when the voltage is 5.97V at a low scale resonant frequency which is 65Hz.

#### Conclusion

In conclusion, energy harvesting from bimorph piezoelectric cantilever beam was studied successfully. Taguchi method was used to optimize the parameter of the energy harvester. An L16 orthogonal array was considered, and simulation of each experiment was run using COMSOL software. It is found that Taguchi method provides cost effectiveness as it reduces the number of experiments in studying the sensitivity effect of the design parameters. In this study, the resonant frequency is inversely proportional to the length of piezo plate. From the results, it was found out that bimorph piezoelectric energy harvester with load resistance of  $10k\Omega$ , width of 17mm and length of 23mm generated 5.97V electric potential and 1.78mW electrical power under the resonance frequency of 65Hz. Despite the energy that harvested from the cantilever is small and in the range of milliwatts, the power was capable to bias some wireless sensors, electronic device, and other low-power applications. For future work on investigating the optimization of unimorph devices is recommended. Therefore, significant differences can be found in the trends between performance and geometric parameters especially when studying the effects of layer thickness, width and length of the piezoelectric.

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